

(Hybrid) Electric Transport Aircraft

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>> *Universally Electric Aircraft*

>> *Hybridization Options*

>> *Boundary Layer Ingestion*

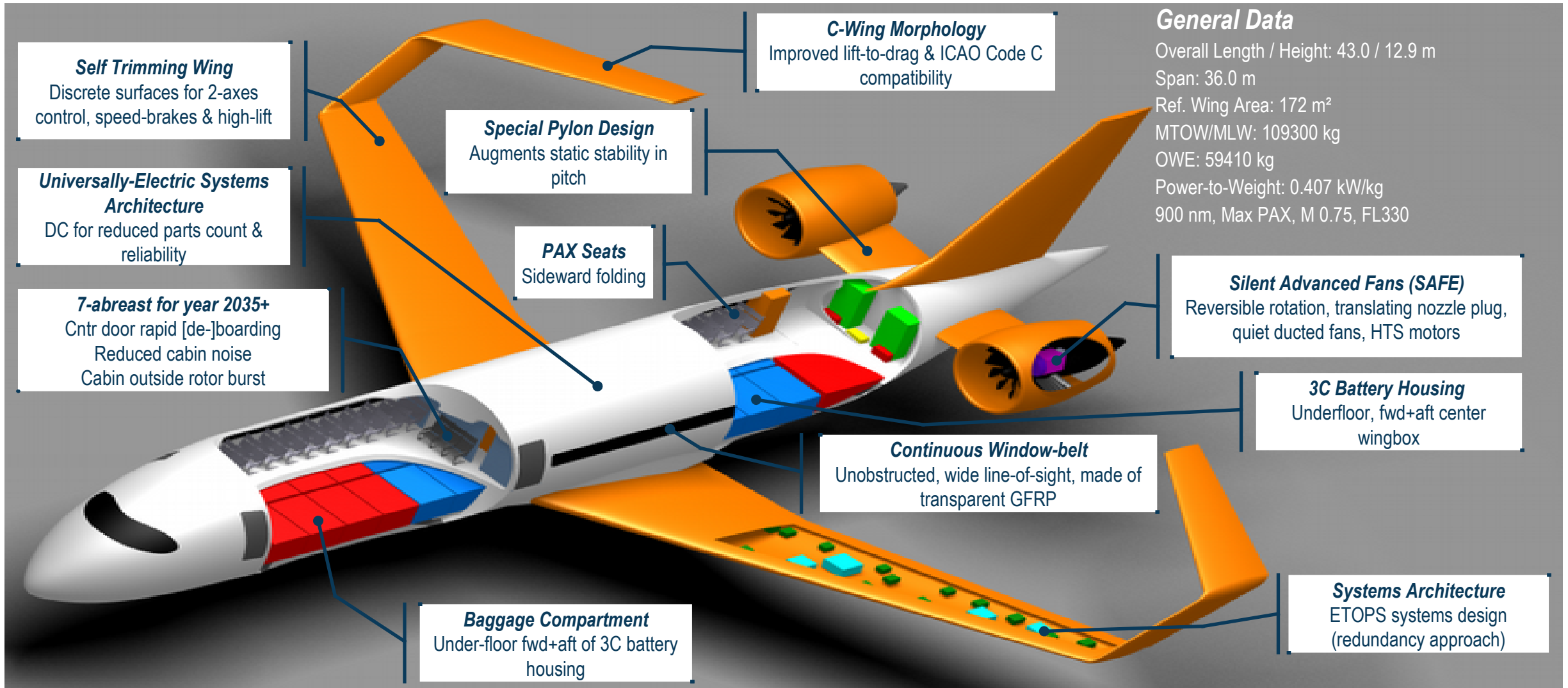


>> **Universally Electric Aircraft**

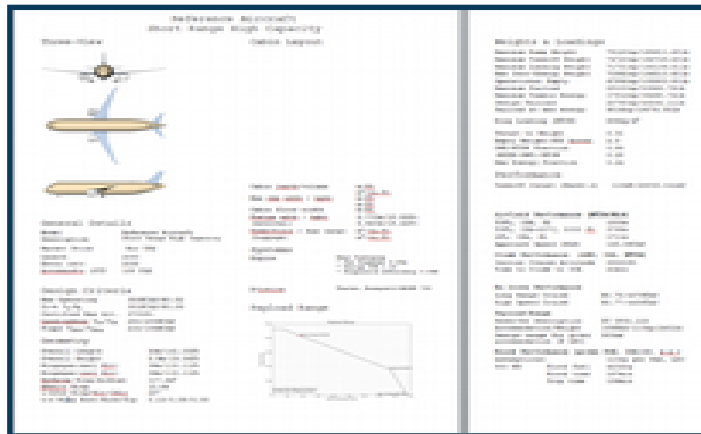
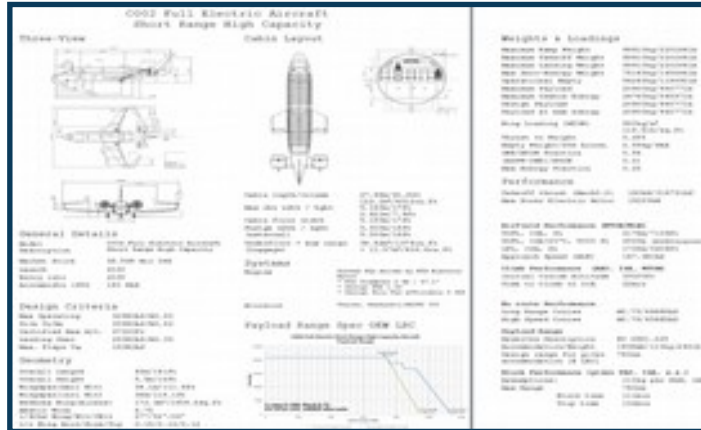
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Benchmarking Ce-Liner



Aircraft Properties	Units	Ce-Liner	B787-3+	Δ (B787-3+)
MTOW	[kg]	109300	73700	+49.1%
MLW	[kg]	109300	70360	N/A
OEW / MTOW	[%]	54.4	65.4	-16.8%
OWE / PAX	kg/PAX	314	253	+24.0%
Max Energy(Fuel) Weight / MTOW	[%]	27.5	24.3	+13.2%
Reference Area (Sref)	[m²]	172.3	115.2	+49.6%
Aspect Ratio (planar wing)	[-]	7.1	10.8	-34.2%
MTOW / Sref	[kg/m²]	635	636	~0.0%
Power / MTOW	[kW/kg]	0.407	N/A	N/A
Thrust / MTOW (M0.20, SL)	[-]	0.233	0.310	-24.8%
TOFL@ISA,SL	[m]	2245	1830	+22.7%
LFL@ISA,SL	[m]	1875	1770	+5.9%
Approach Speed (MLW)	KCAS	149	146	+2.1%
Des.Range, LRC, ICA, Max-PAX	[nm]	900 nm, M0.75, FL330		
(L/D) @ LRC, TOC, ISA+10°C	(-)	20.5	18.4	+11.4%
ESAR, 900 nm, LRC, ISA+10°C	[km/kWh]	0.0473	0.0374	+26.4%

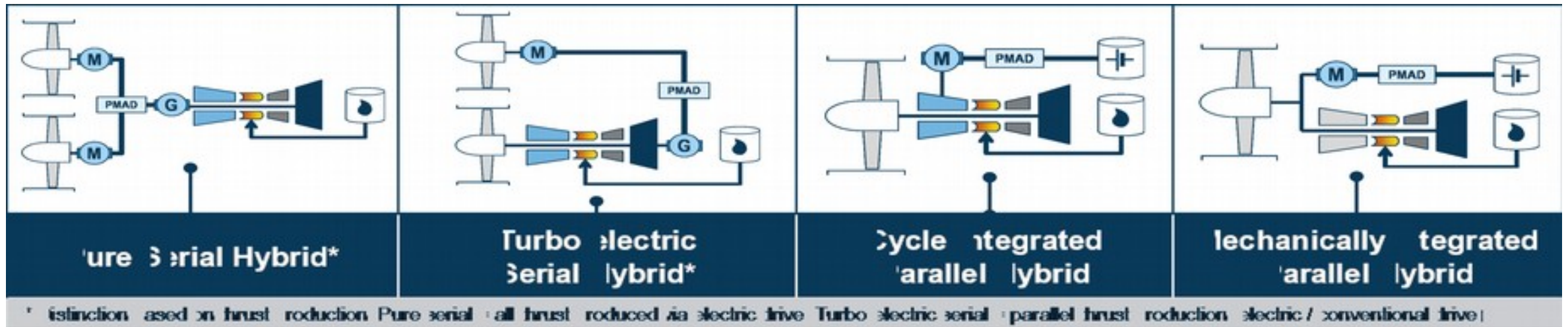
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>> Four Basic Approaches to Hybrid Electric Propulsion



>> Important system descriptors

> Degree of power hybridization H_p

$$H_p = \frac{P_{\text{supply,elec}}}{P_{\text{supply,tot}}} = \frac{P_{\text{supply,elec}}}{P_{\text{supply,elec}} + P_{\text{supply,fuel}}}$$

> Degree of energy hybridisation H_E

$$H_E = \frac{E_{\text{supply,elec}}}{E_{\text{supply,tot}}} = \frac{E_{\text{supply,elec}}}{E_{\text{supply,elec}} + E_{\text{supply,fuel}}}$$

Parallel Hybrid (A/C Level)

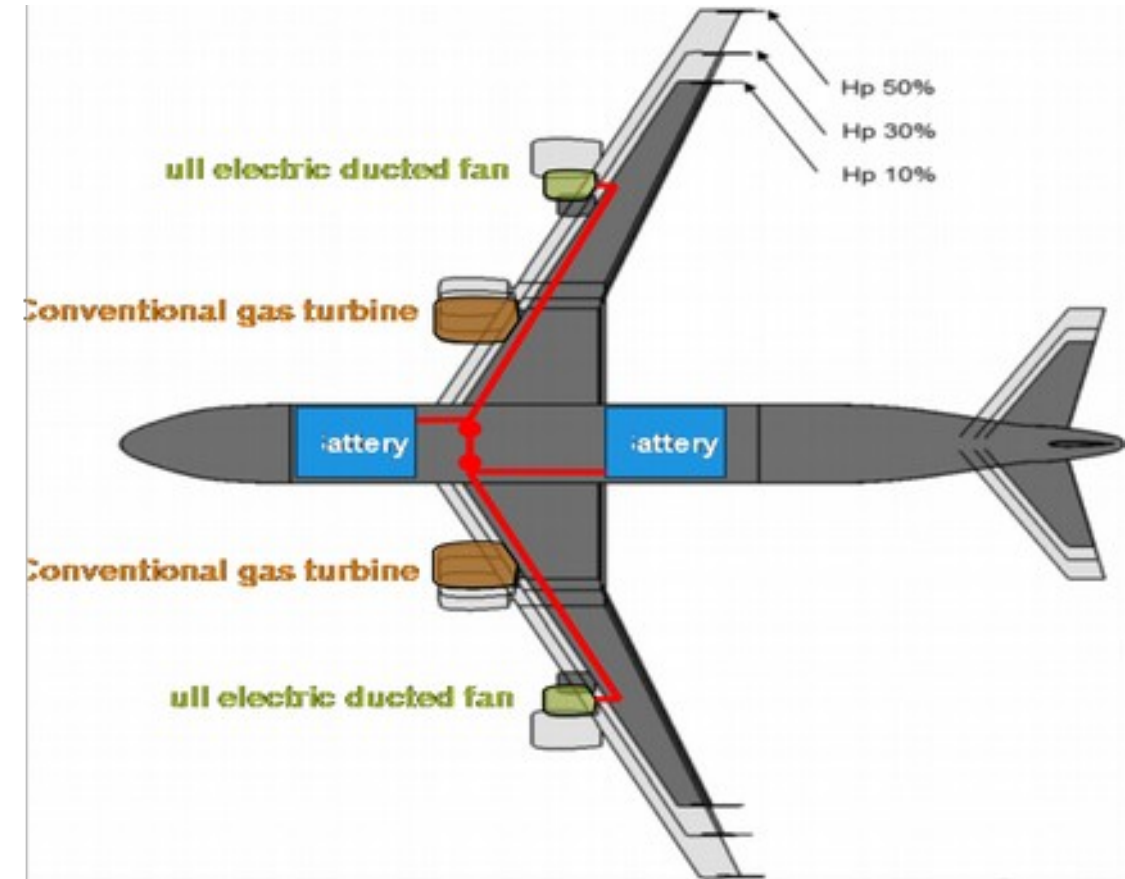
>> Hybrid-electric propulsion system with 4 propulsors

- > 2 conventional gas turbines
- > 2 electrically powered ducted fans
- > No direct coupling between different energy carriers/propulsion systems

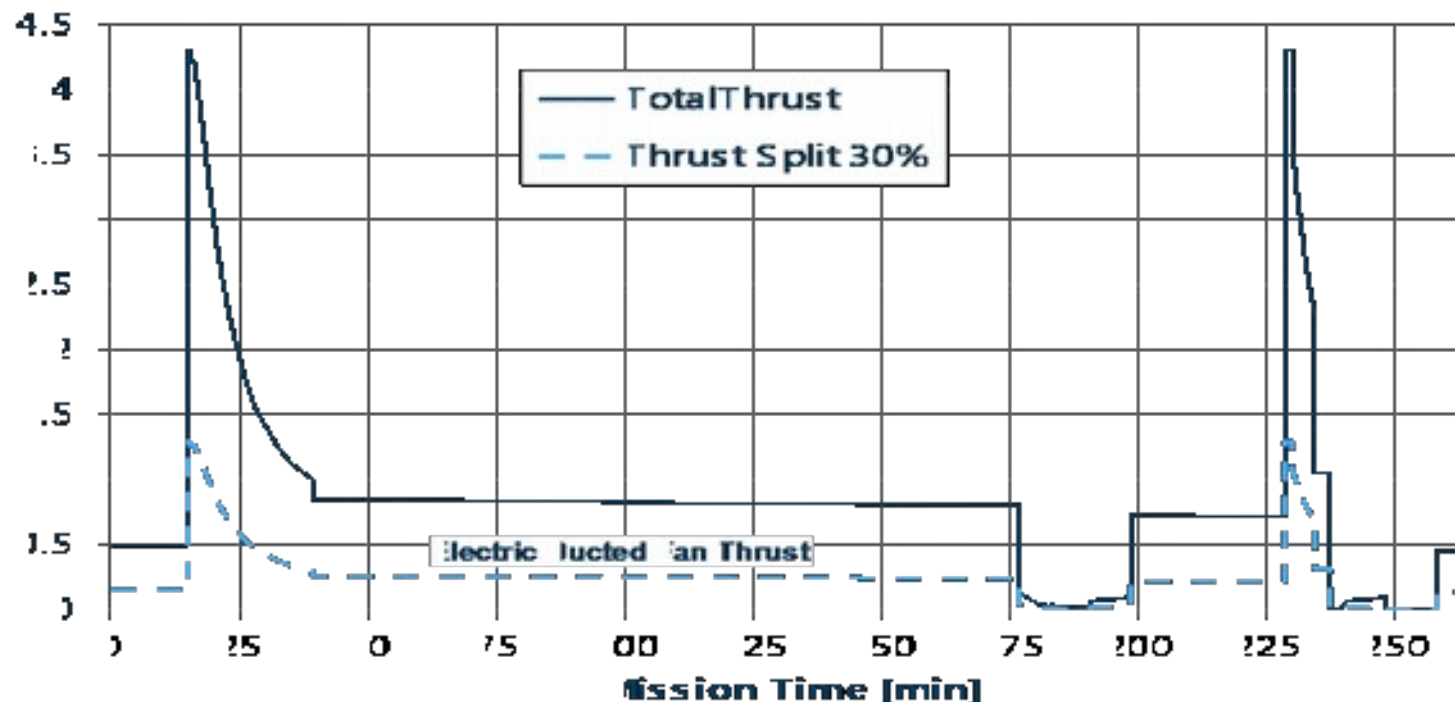
>> Battery supplied electric system used as assistance system

>> Expected advantages

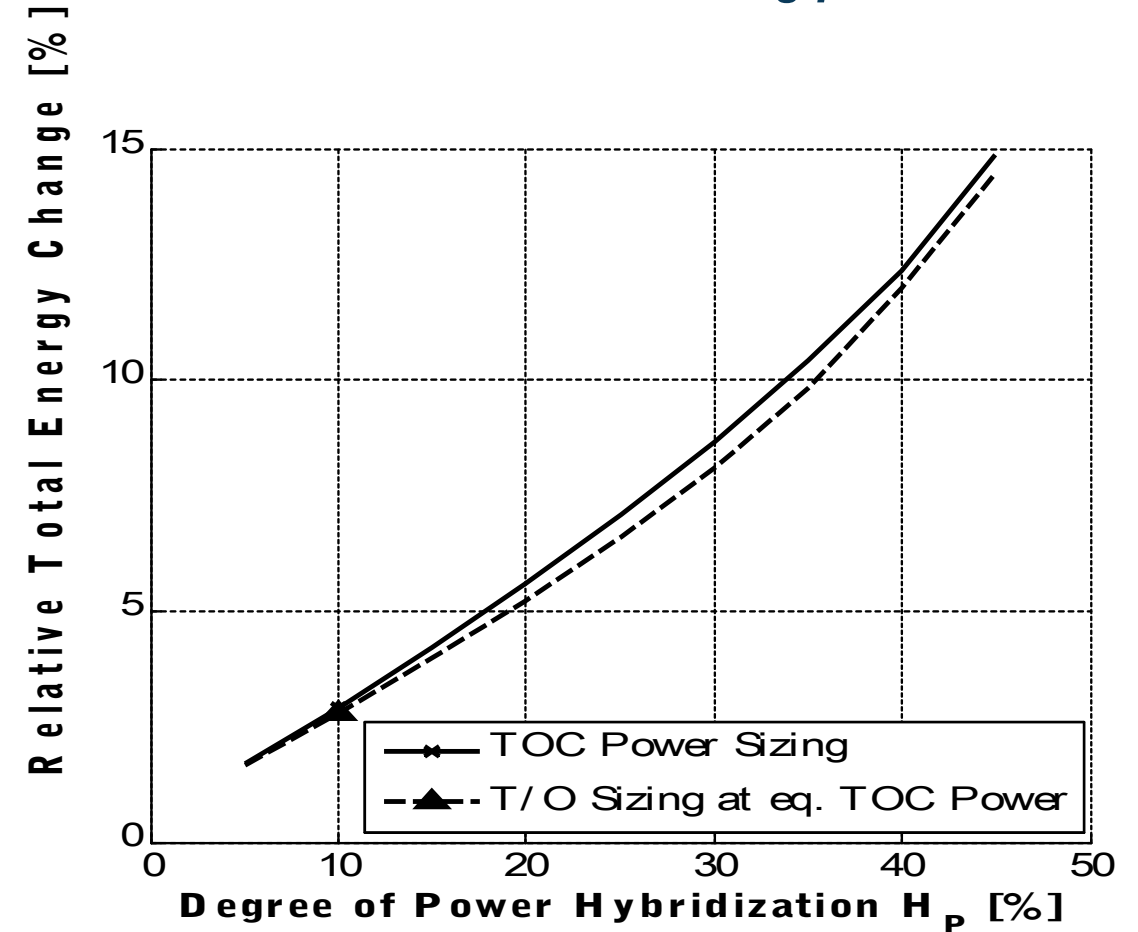
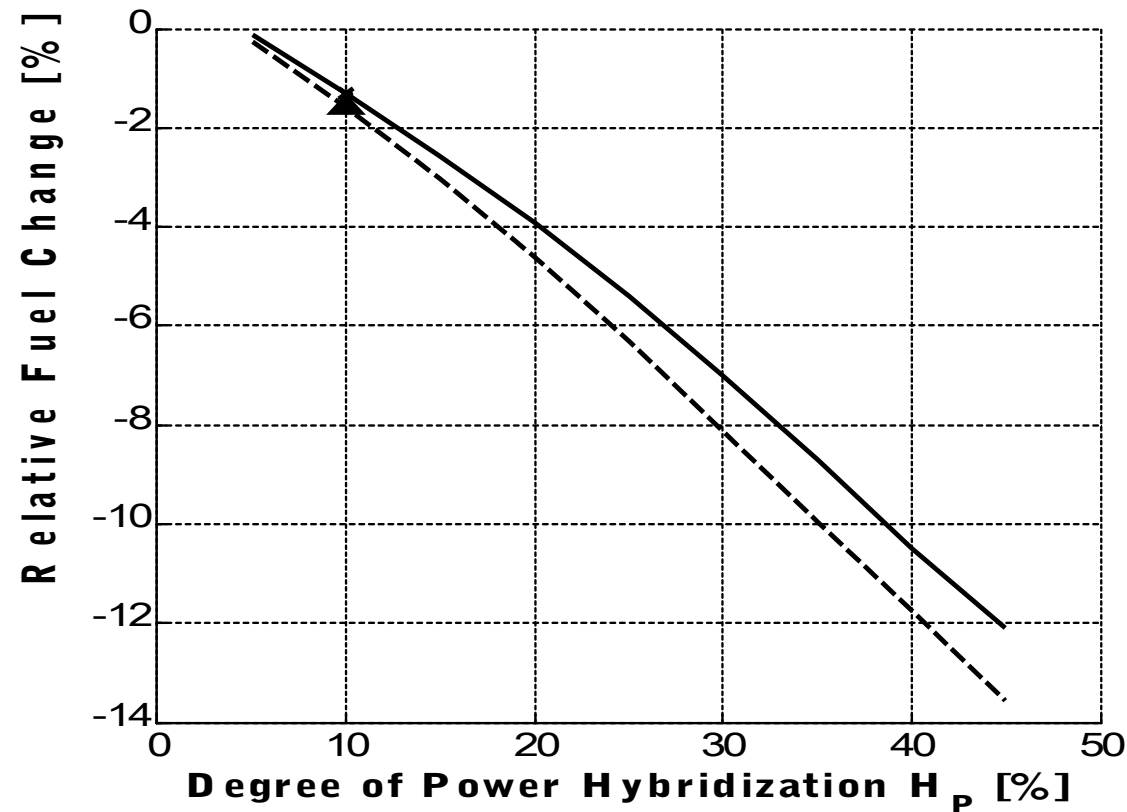
- > Downsizing of gas turbines
- > Electric cruise capability
- > Increased operational behavior compared to integrated parallel hybrid topologies → No coupling of propulsors



- >> *Electric support given by constant thrust split between conventional and electric supplied propulsors over the entire mission*
- >> *Normalized power profile used to determine fuel and battery demand*
- >> *Aircraft level assessment performed with the help of trade factors*



➤➤ *Impact of different values of degree of power hybridizations and electric motor sizing points on the in-flight fuel burn and mission energy*

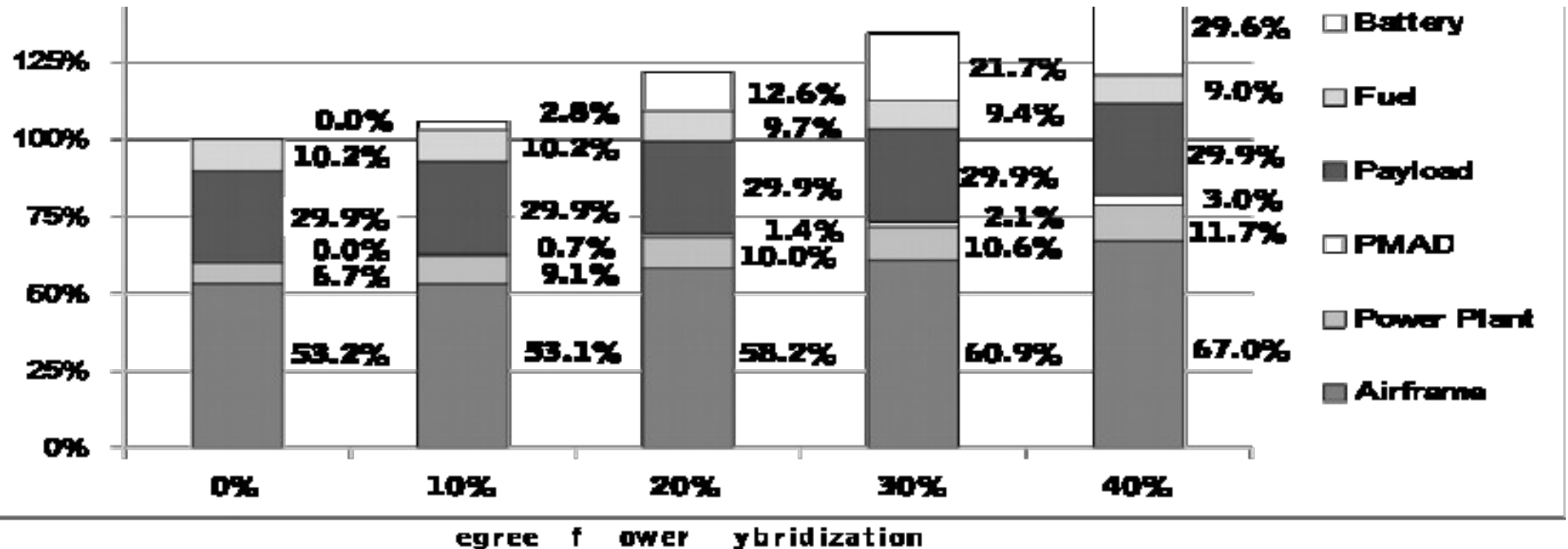


Initial Aircraft Level Results and Sensitivities I

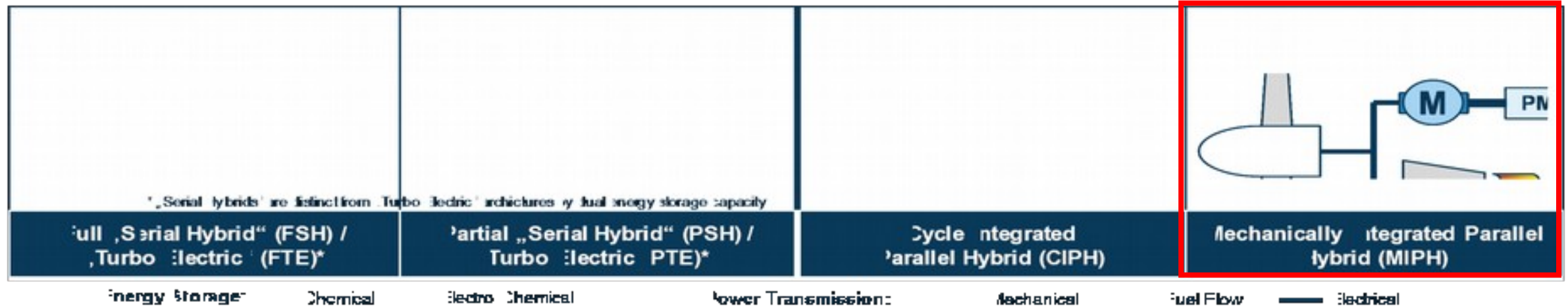
>> Assuming a 1000 Wh/kg battery for different values of degree of power hybridization for a 1300nm and 180 PAX mission results in

> up to 50% higher MTOW

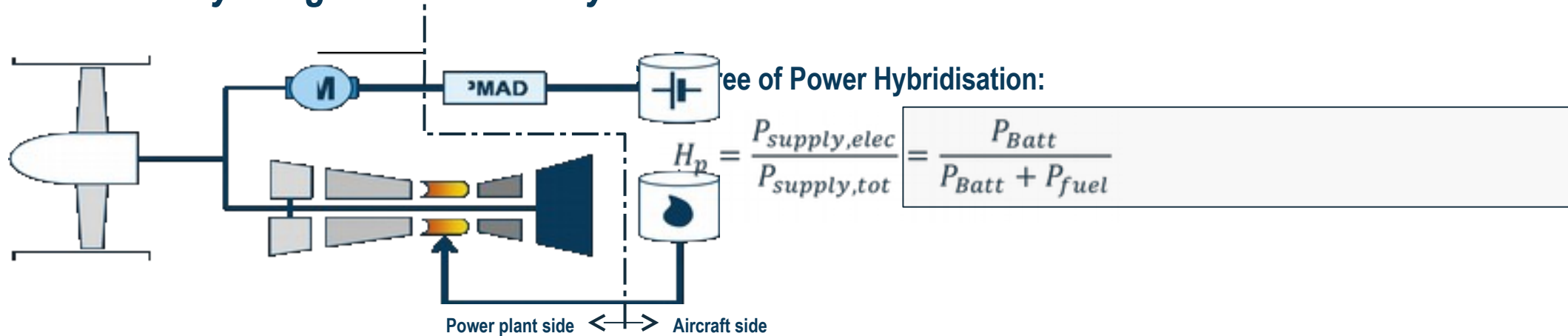
> up to 11.7% lower in-flight fuel burn, but 12.4% higher mission energy demand



Hybrid-electric Propulsion Landscape



>> *Mechanically Integrated Parallel Hybrid:*

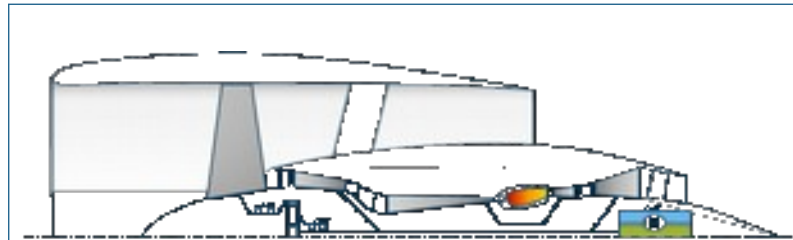
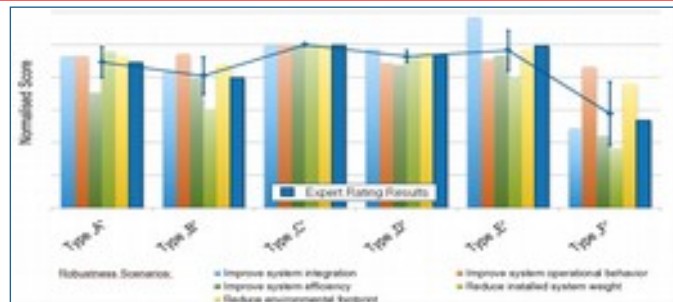


>> MIPH application:

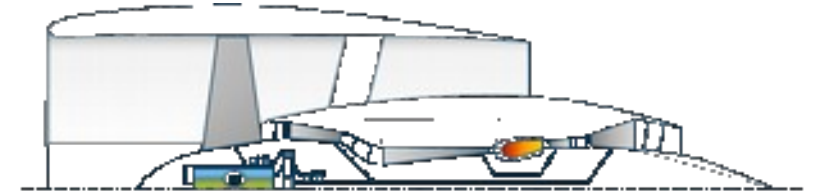
- > UHBR short range GTF
- > 20klbf thrust class

Selected concept

- + High speed electric motor
- + Thermal environment for electronics
- + Overall most robust solution



Type A Electric machine integrated behind PT, motor connected to PT shaft



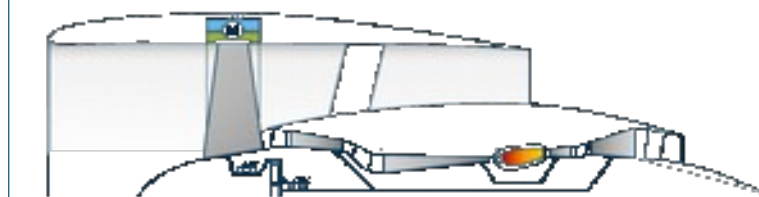
Type B Electric machine integrated with fan hub, motor connected to fan shaft



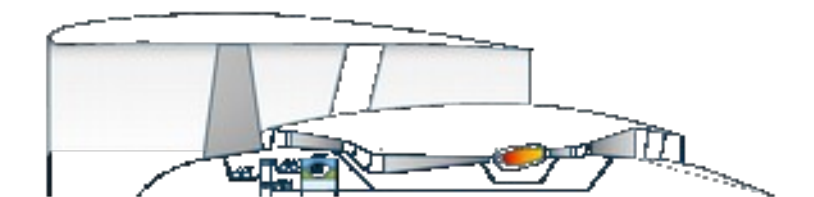
Type C Electric machine integrated with fan hub, motor connected to PT shaft



Type D Electric machine encircling core engine, motor connected to PT shaft via coupler

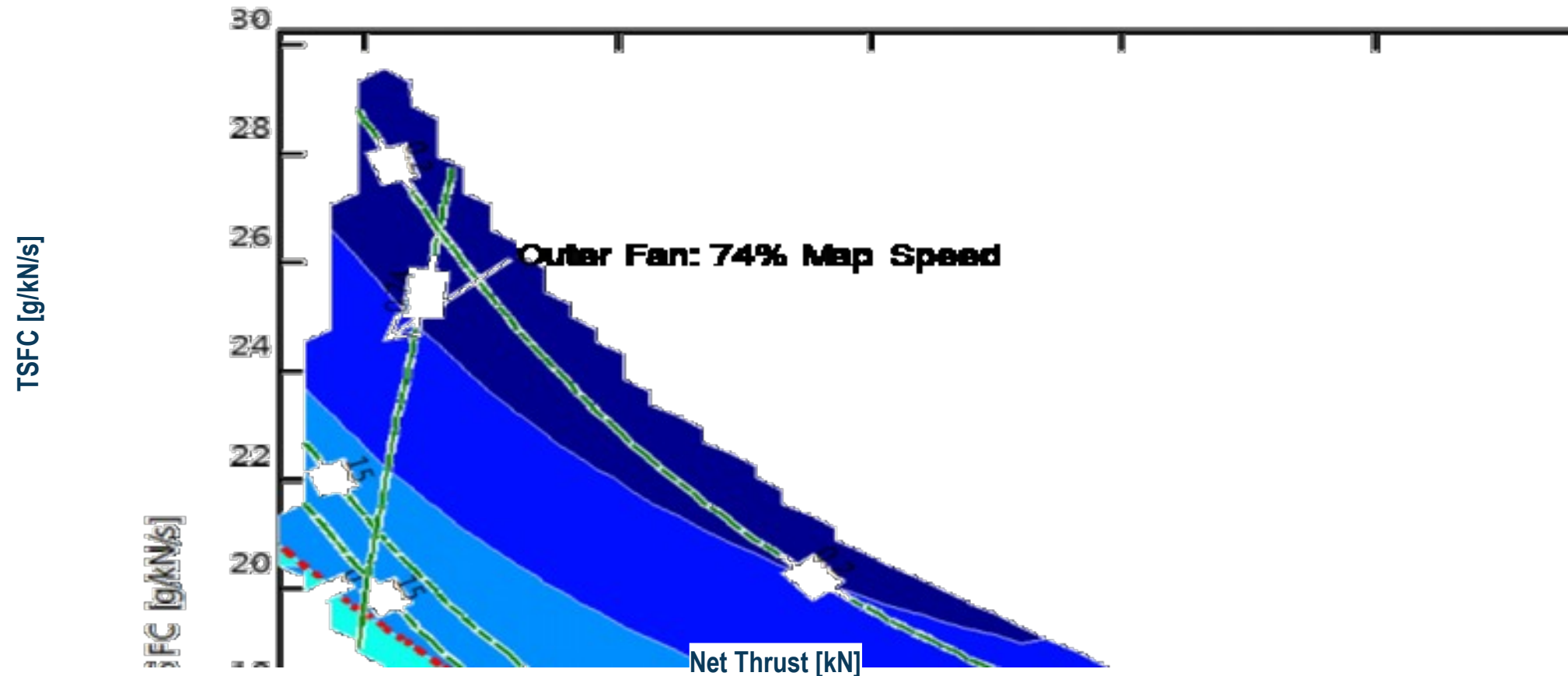


Type E Electric machine integrated with fan using quasi-rigid fan motor tip drive

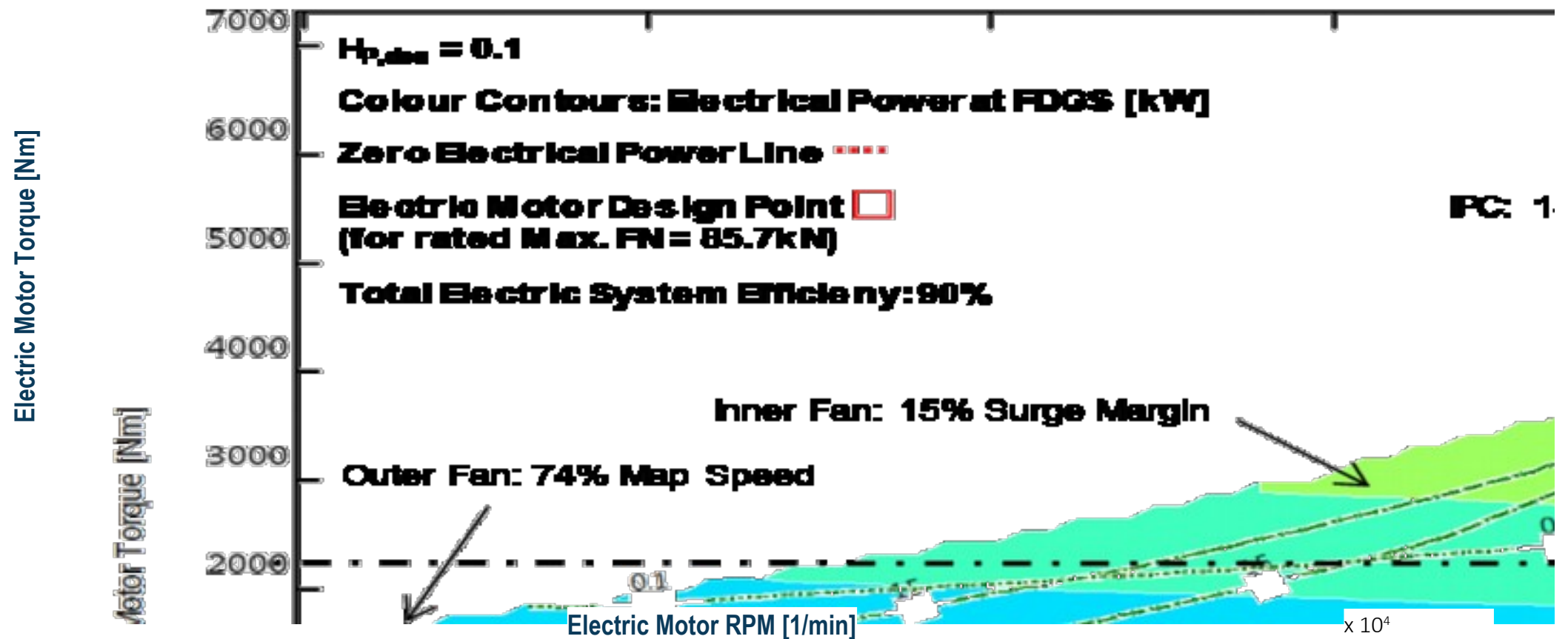


Type F Electric machine integrated behind fan drive gear system, motor connected to gear, fan connected to another gear

>> Cruise part power characteristics for S/R GTF application ($H_{P,des}=0.1$)

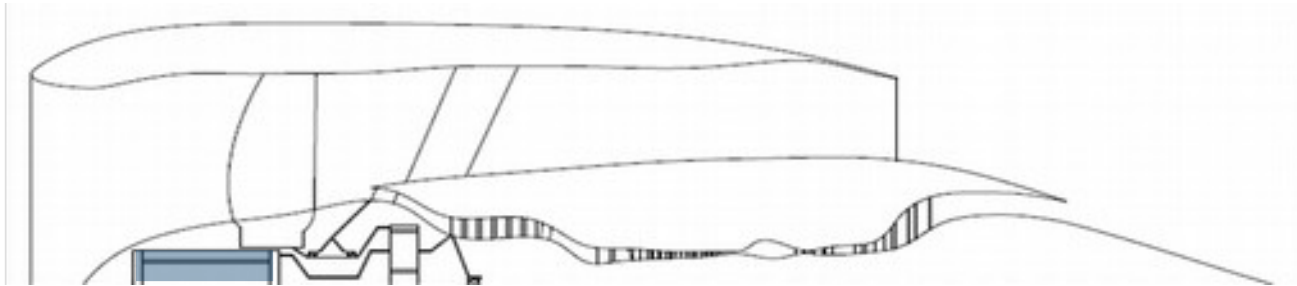


>> Sizing point take-off for ENOVAL S/M range application ($H_{P,des}=0.1$)

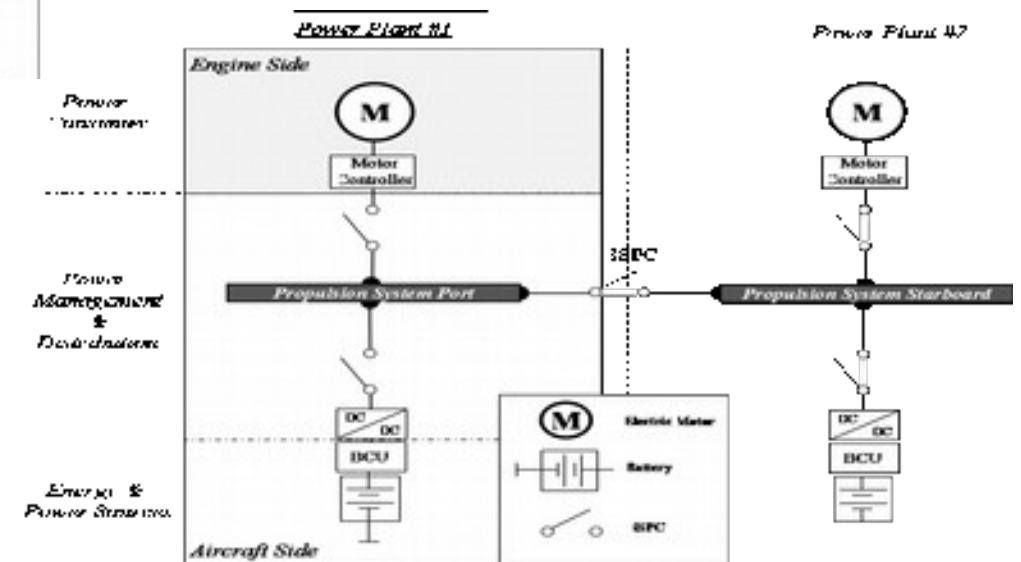


>> Basic flow path of mechanically integrated parallel hybrid power plant

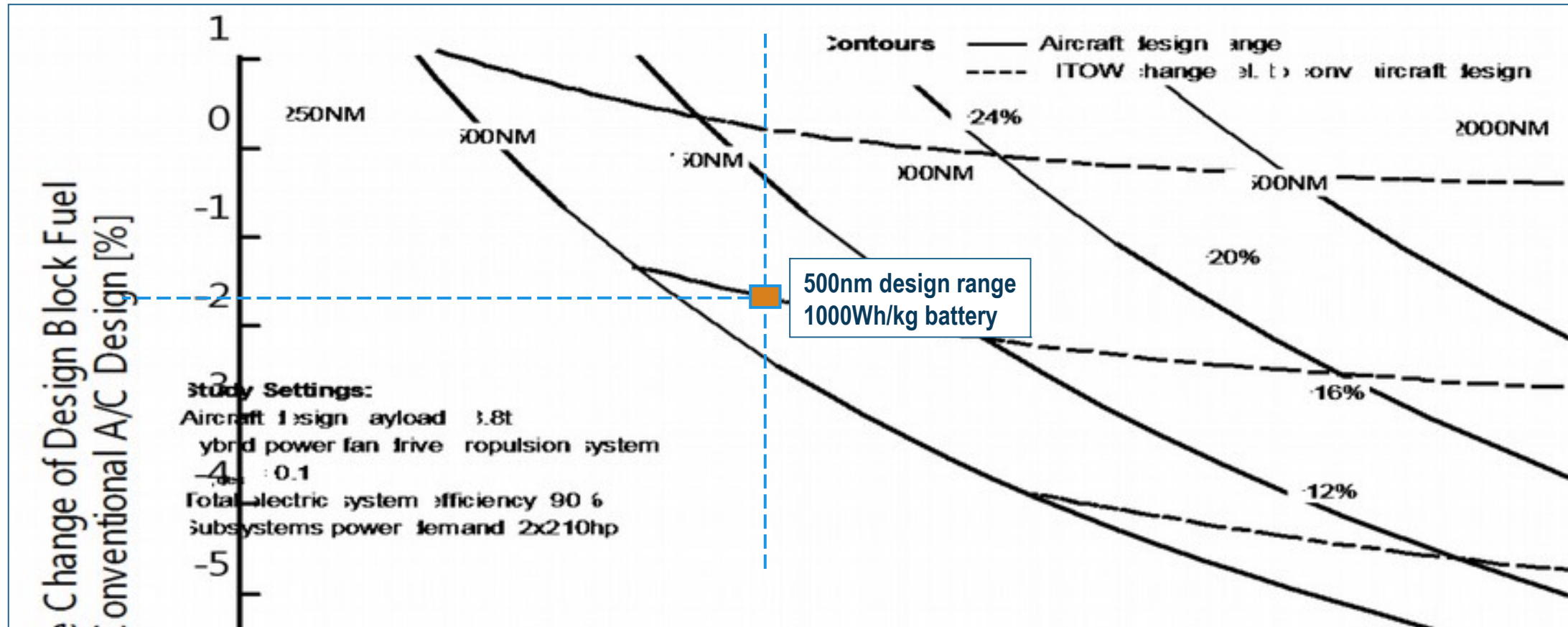
- > $H_{P,des} = 0.1$
- > 2MW electric motor



>> **Layout of electrical system architecture:**



>> Mechanically integrated parallel hybrid vs. advanced turbofan technology



>> Weight breakdowns for MIPH and advanced turbofan technology powered aircraft, designed for a 500NM stage length:

Weight Item	Conventionally powered A/C	MIPH turbofan powered A/C ¹	Delta [%]
Airframe structures and systems	30811	33126	+7.5
Power plant systems ²	6822	7780	+14.0
Electric systems architecture	n/a	2270	n/a
Battery system	n/a	5330	n/a
OWE	37633	48506	+28.9
Payload	18775	18775	±0.0
Design fuel	3839	3706	-3.5
MTOW	60247	70986	+17.8

¹ 1000Wh/kg battery system specific energy

² weight of electric motors included in electric systems architecture

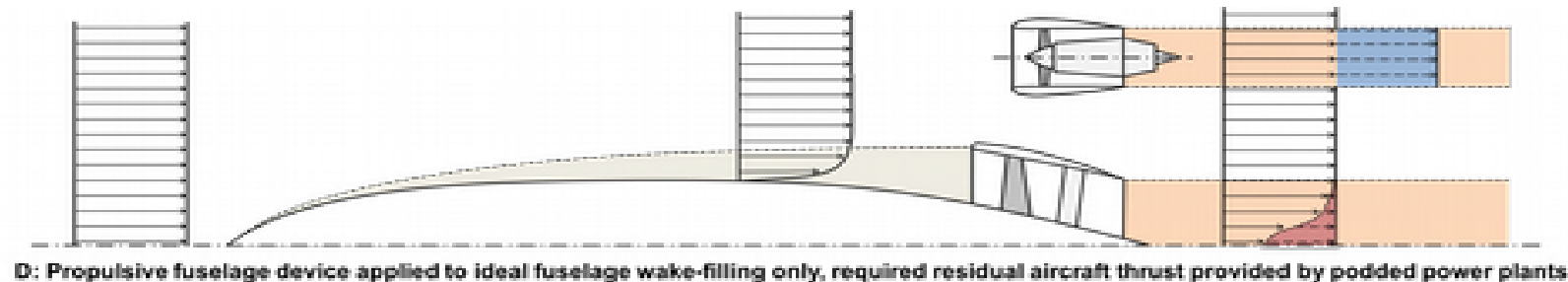
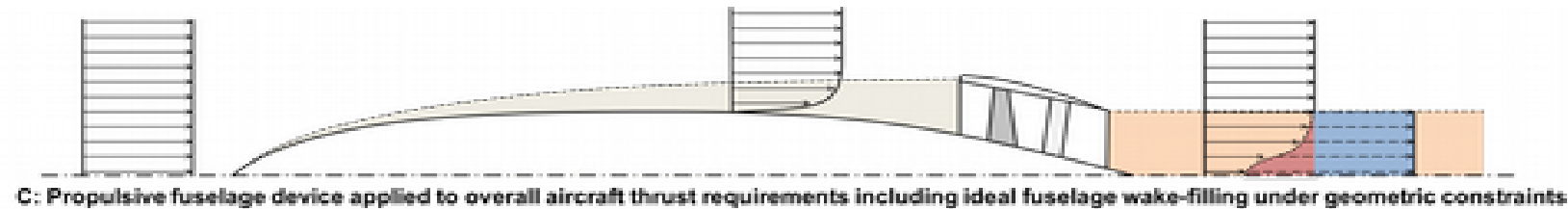
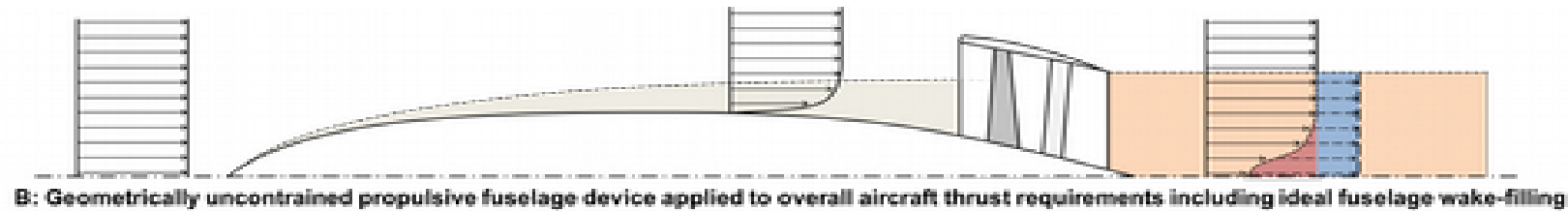
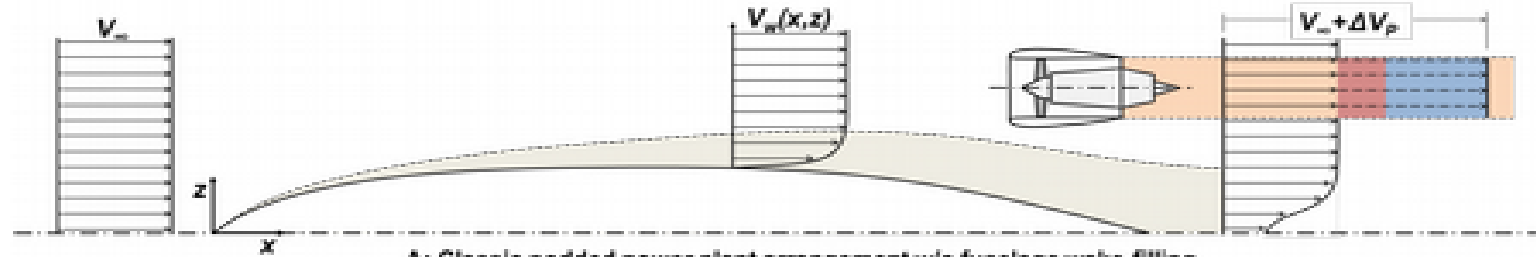
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>> **Boundary Layer Ingestion**



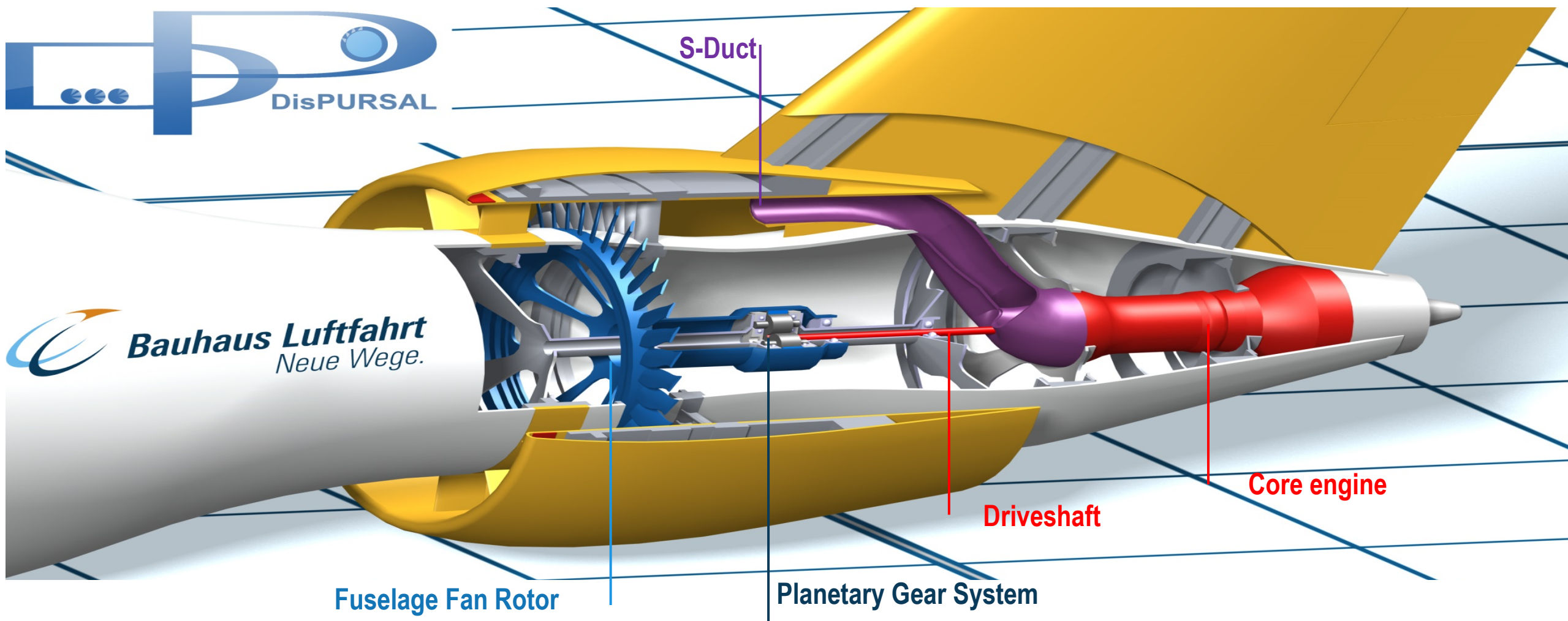
The Principle of Aircraft Wake Filling



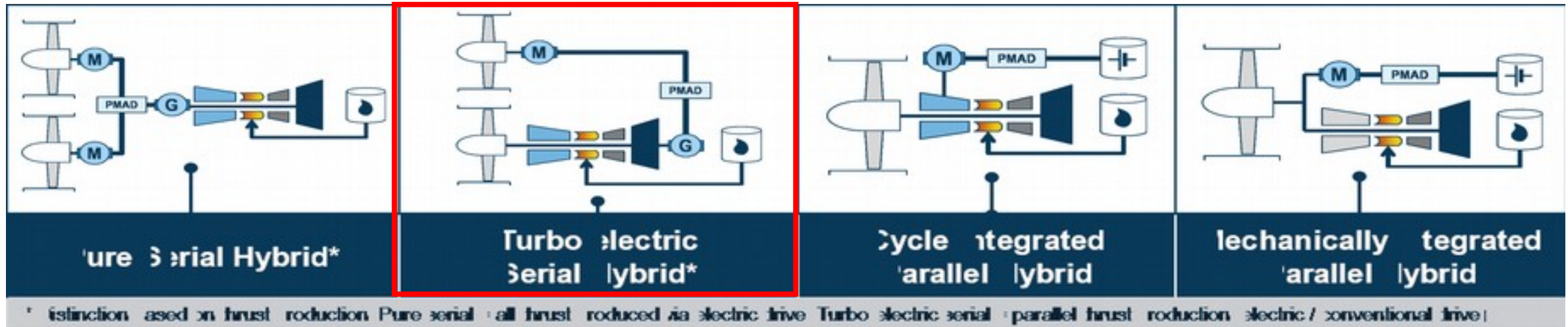
Legend:

-  Fuselage boundary layer
-  Propulsion system jet flow field
-  Jet momentum equivalent for ideal fuselage wake compensation
-  Jet momentum equivalent for aircraft residual thrust requirement

Fuselage Fan Propulsion System Integration



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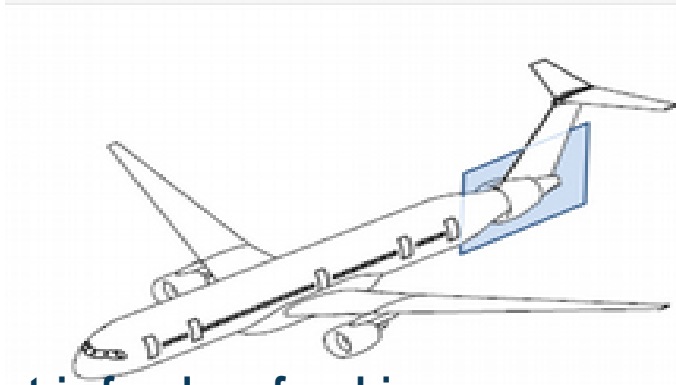
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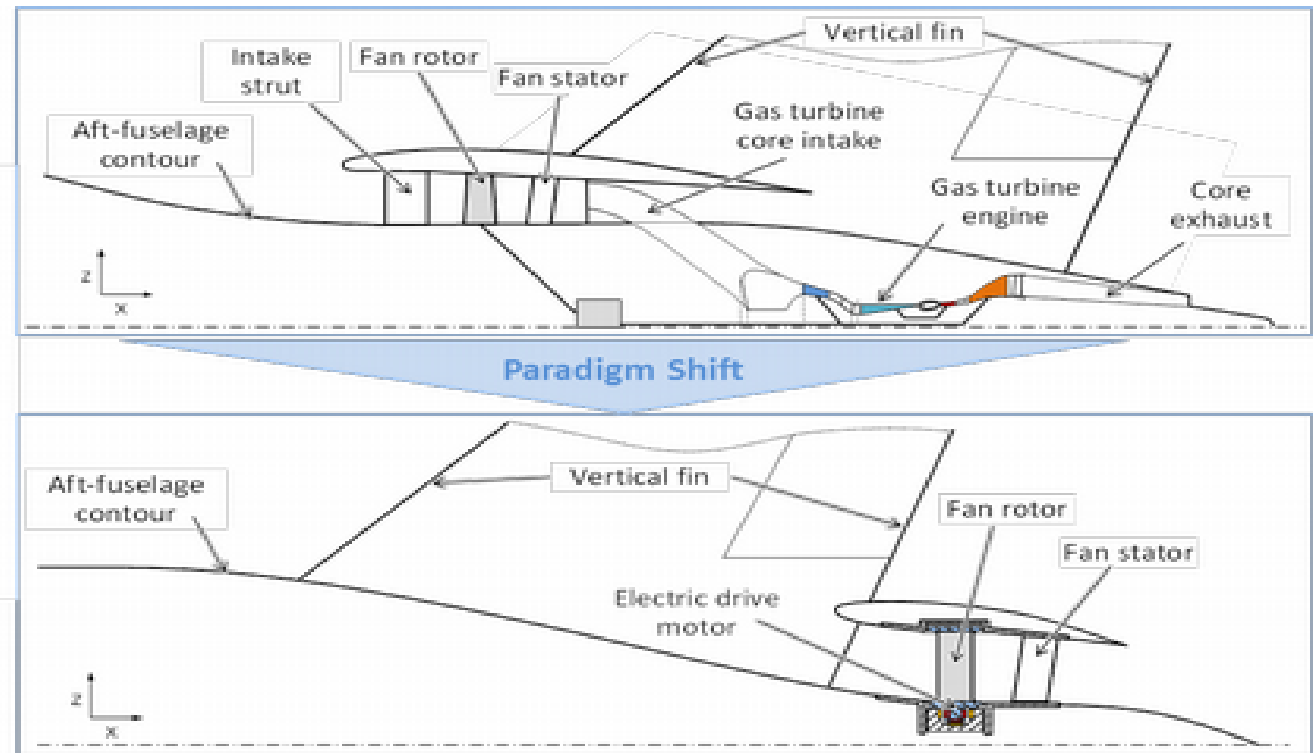
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>> Wake-filling aft-fuselage propulsion integration with turbo-electric design paradigm shift

- > Mechanical fuselage fan drive
- > DisPURSAL: **-9% Design Fuel**



- > Turbo-electric fuselage fan drive
- > Init. Estimate: **-11% Design Fuel**



Ref.: Seitz, A. „Power Train Options for a Propulsive Fuselage Aircraft Layout, Presentation at MEA-USA Conference, Seattle, August 2016

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